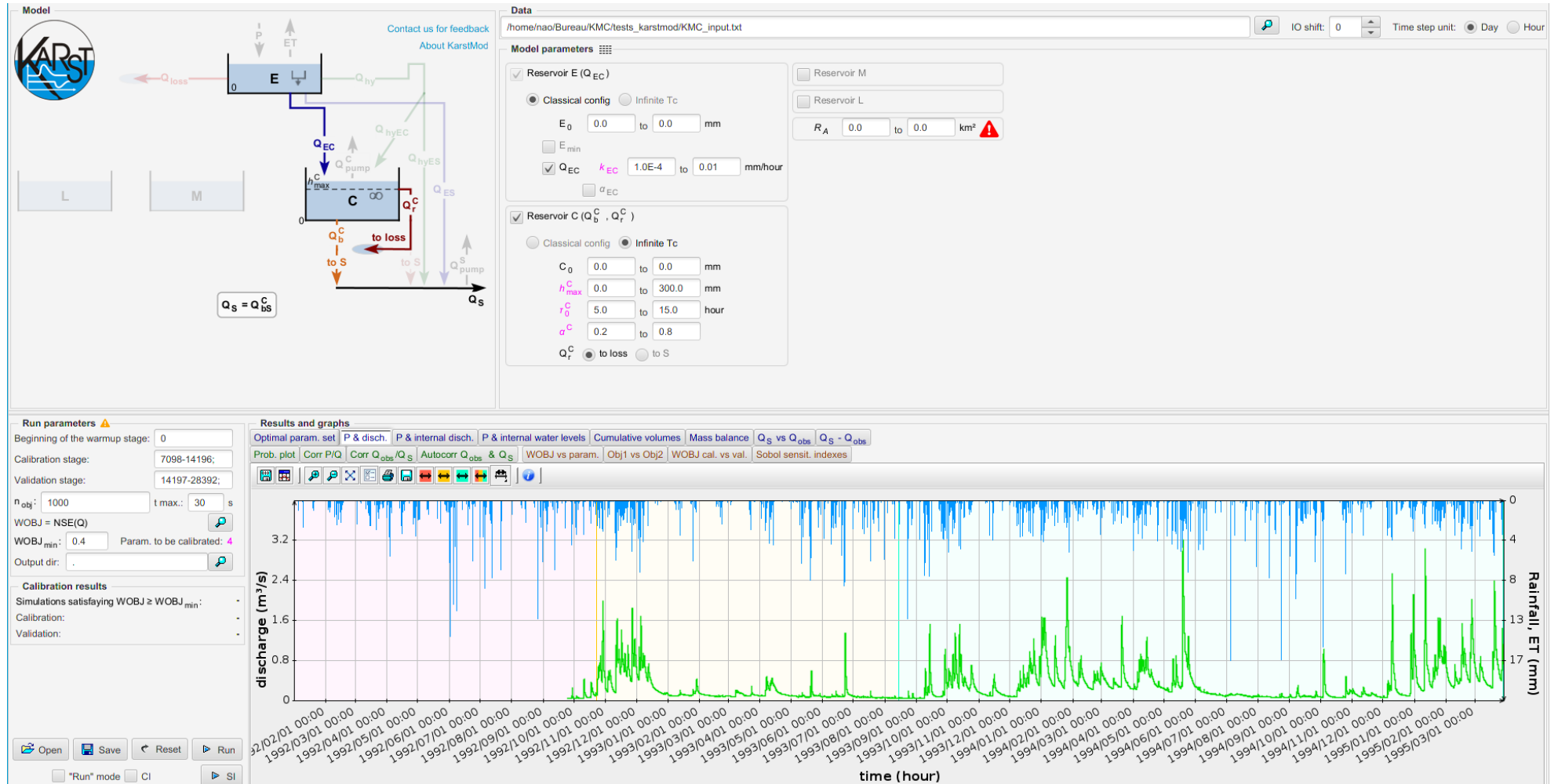
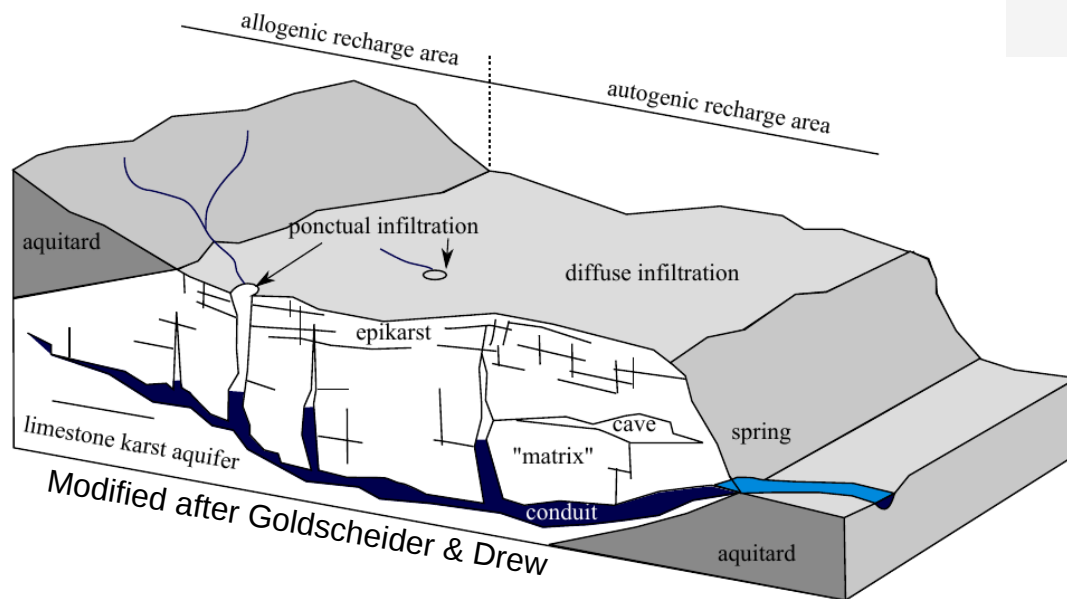
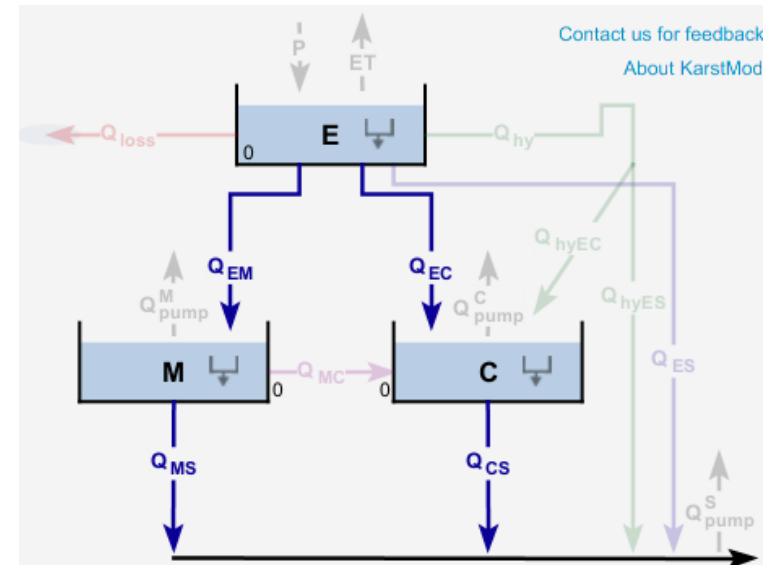


KarstMod platform : an overview



1D compartment models



Operational :

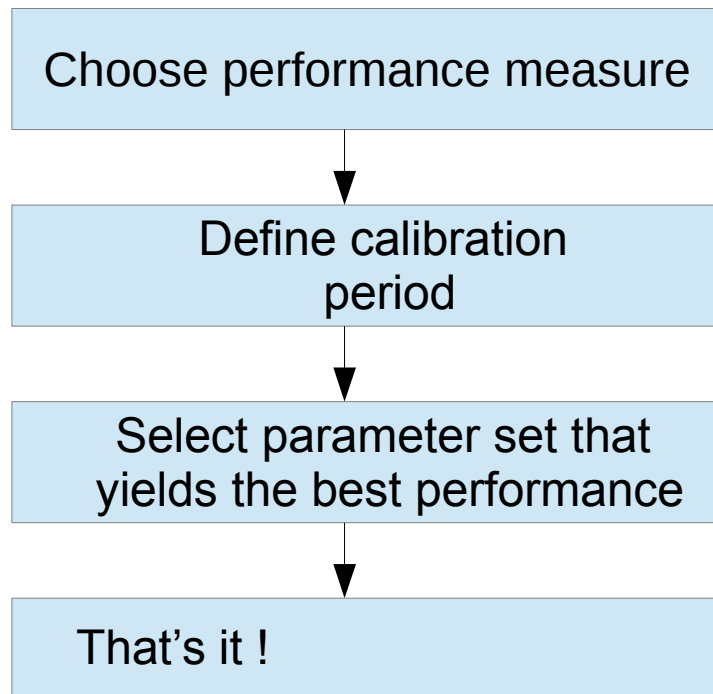
→ Forecast of system response

Research

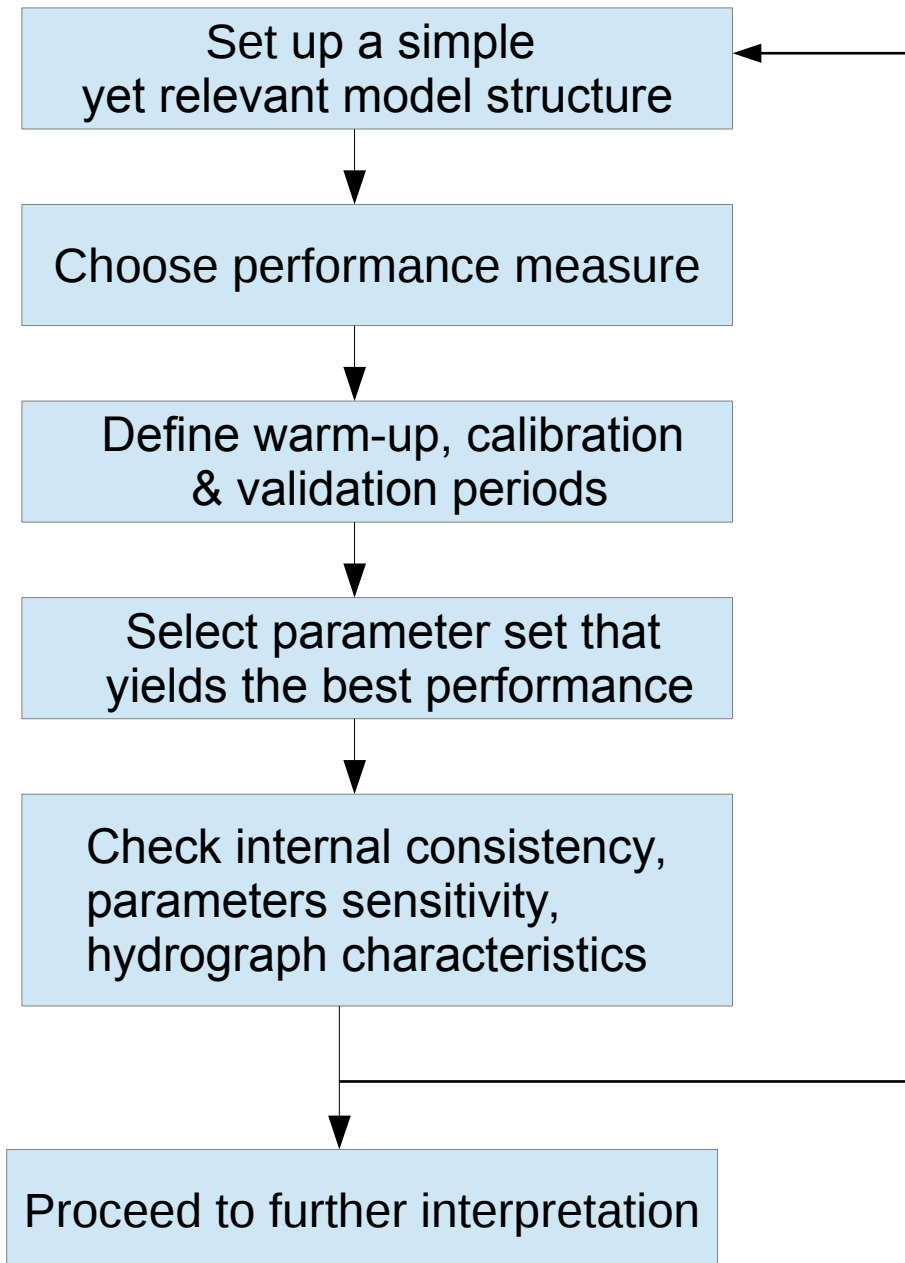
→ Understanding of the main processes at stake

→ Insights into internal behaviour

Modelling workflow



Modelling workflow



Start simple !
Do you data really supports your model ?
Gradual complexification approach

Model

KARST

Contact us for feedback
About KARSTmodel

Diagram illustrating a three-reservoir system (E, M, C) and a lake (L). The system is defined by the following flows and parameters:

- Reservoir E (Evaporation/Transpiration):**
 - Inflows: P (precipitation), ET (evaporation/transpiration).
 - Outflows: Q_{ES} (to lake L), Q_E (to reservoir M), Q_{EC} (to reservoir C).
- Reservoir M (Mountain/Storage):**
 - Inflows: Q_E (from reservoir E).
 - Outflows: Q_{EM} (to lake L), Q_{MS} (to reservoir C).
- Reservoir C (Catchment/Storage):**
 - Inflows: Q_{EC} (from reservoir E), Q_{MS} (from reservoir M).
 - Outflows: Q_{BCS} (to lake L), Q_{CS} (to lake L), Q_{ES} (to lake L).
- Lake L:**
 - Inflows: Q_{ES} (from reservoir E), Q_{EM} (from reservoir M), Q_{BCS} (from reservoir C), Q_{CS} (from reservoir C).
 - Outflows: Q_S (to the sea).

The diagram also includes a 'Model' logo and contact information for KARST.



- Provide a friendly environment of 1D rainfall / water level / discharge modelling
- Provide analytical solutions, whenever possible
- Promote good modelling practices

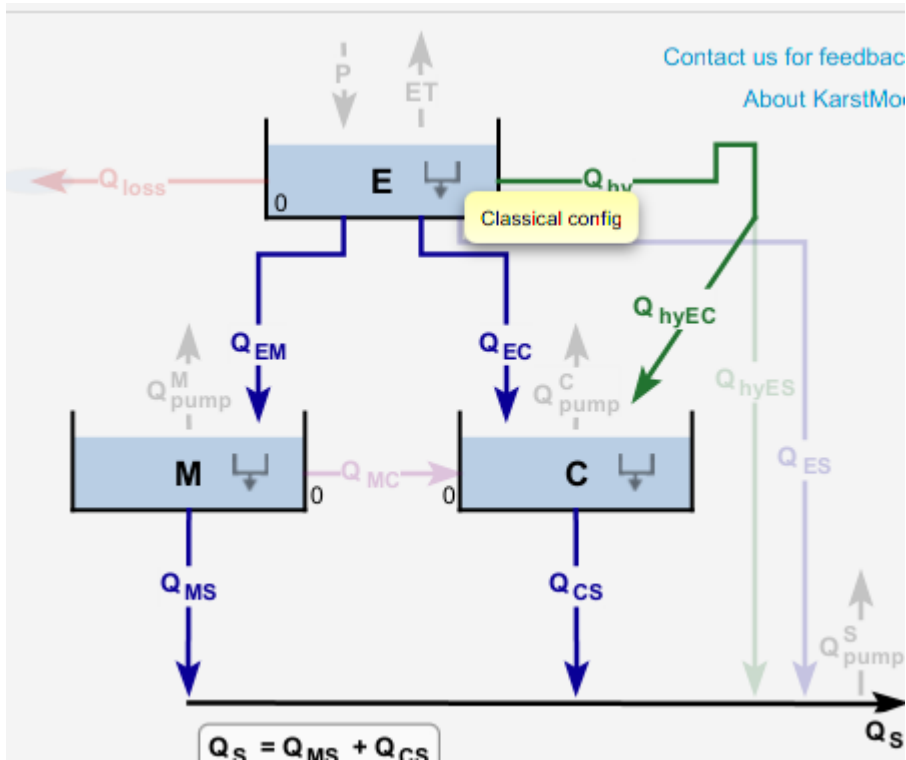
Start simple !
Do your data really support your model ?
Gradual complexification approach

Step by Step example

- KarstMod_2.2.0.r.jar
- Java Runtime Environment 64 bits ≥ 1.8
- KarstMod user manual
- Input file : FontaineVaucluse1994_2000.txt



Step by Step example : structure selection



2 configurations allowed for each compartment

- Classical configuration (Maillet-type law)
- Infinite characteristic time transfer function

Start simple !

Do your data really support your model ?
Gradual complexification approach

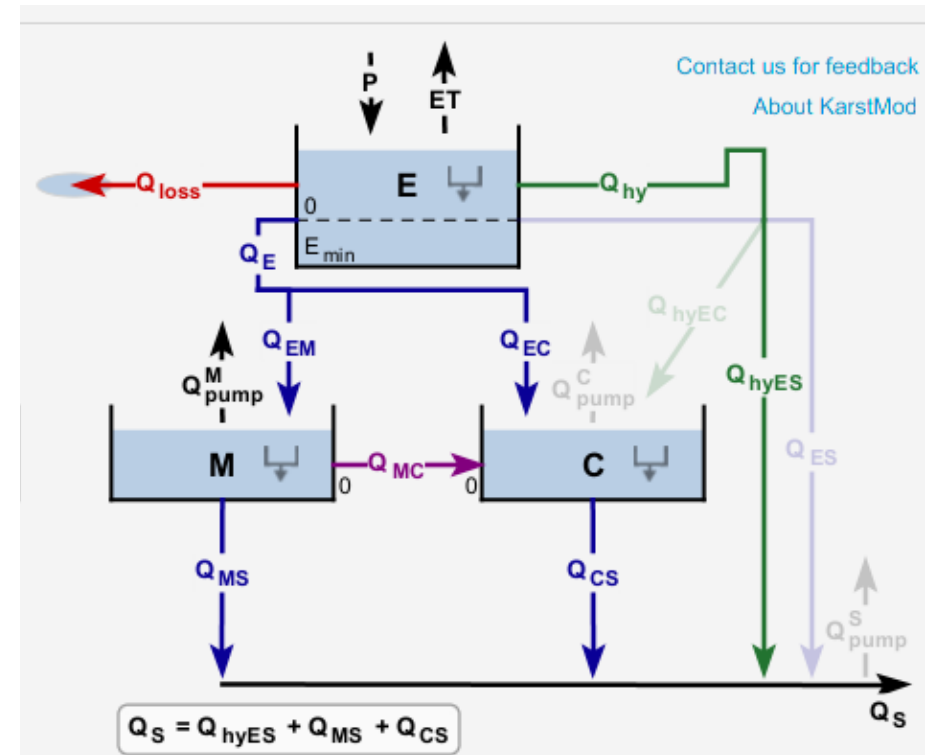
Step by Step example : transfer laws

Classical configuration

- Linear discharge law
- Non-linear discharge law
- Activation thresholds
- Soil available water content
- Pumping / Losses
- Hysteretic discharge law
- M-C interaction

$$Q_{AB}(t) = k_{AB} \times A(t)$$

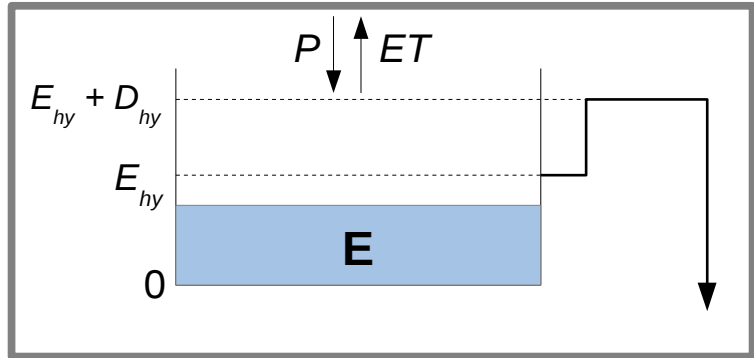
$$Q_{AB}(t) = k_{AB} \times A(t)^{\alpha_{AB}}$$



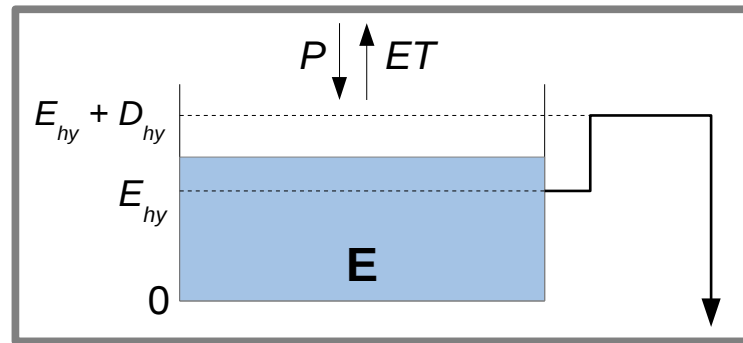
Step by Step example : transfer laws

Classical configuration : Hysteretic discharge law $Q_{hy}(t) = k_{HY} (E - E_{hy})^\alpha$

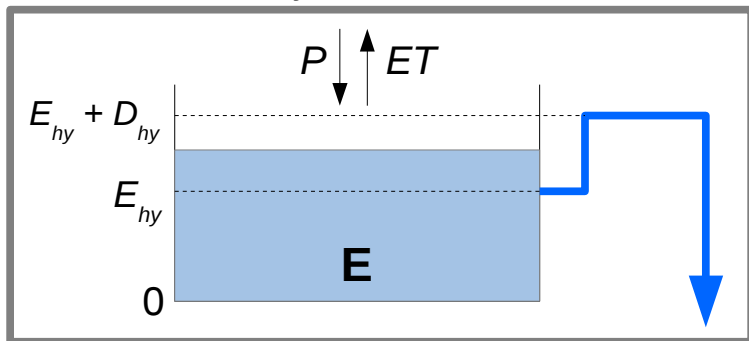
Step 1, $E < E_{hy}$, deactivated hysteretic flow



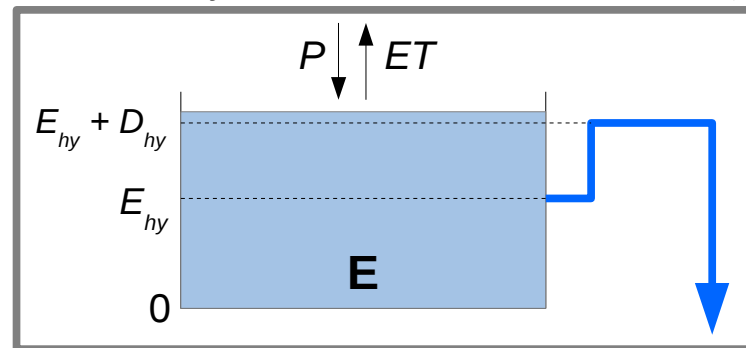
Step 2, $E > E_{hy}$
Still deactivated hysteretic flow



Step 3, $E_{hy} < E < E_{hy} + D_{hy}$
Activated hysteretic flow



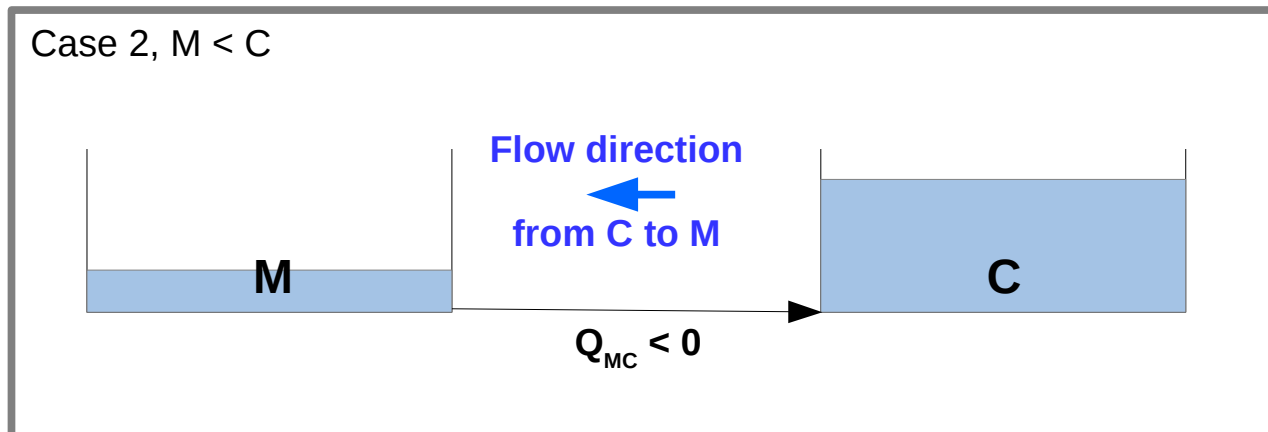
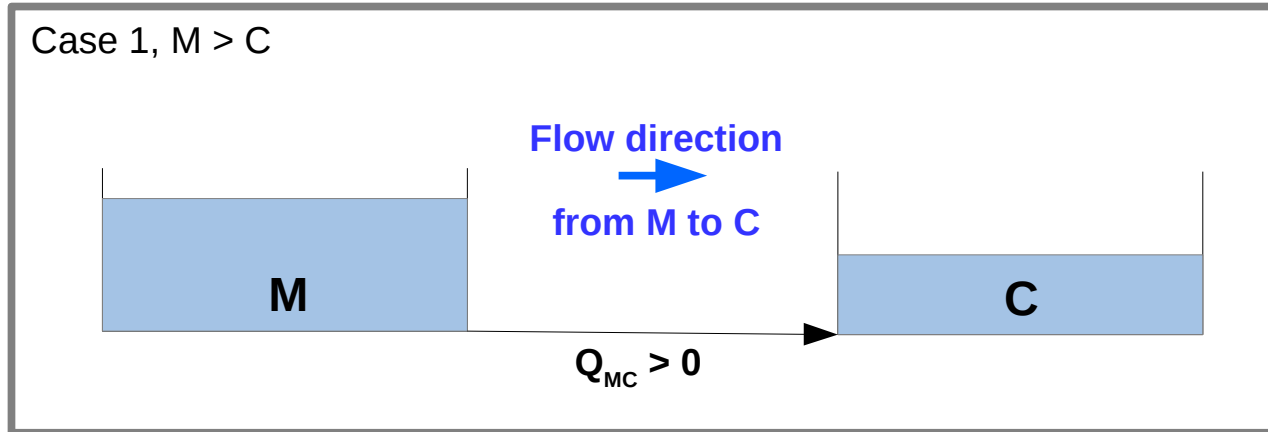
Step 3, $E > E_{hy} + D_{hy}$
Activated hysteretic flow



Activation of discharge law depends on prior state of saturation

Step by Step example : transfer laws

Classical configuration : Inter-compartments discharge law $Q_{MC}(t) = k_{MC}(M - C)^\alpha$



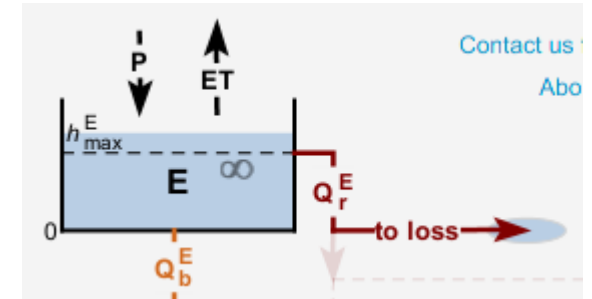
Flow direction depends on relative water levels between compartments

Step by Step example : transfer laws

Infinite characteristic time configuration

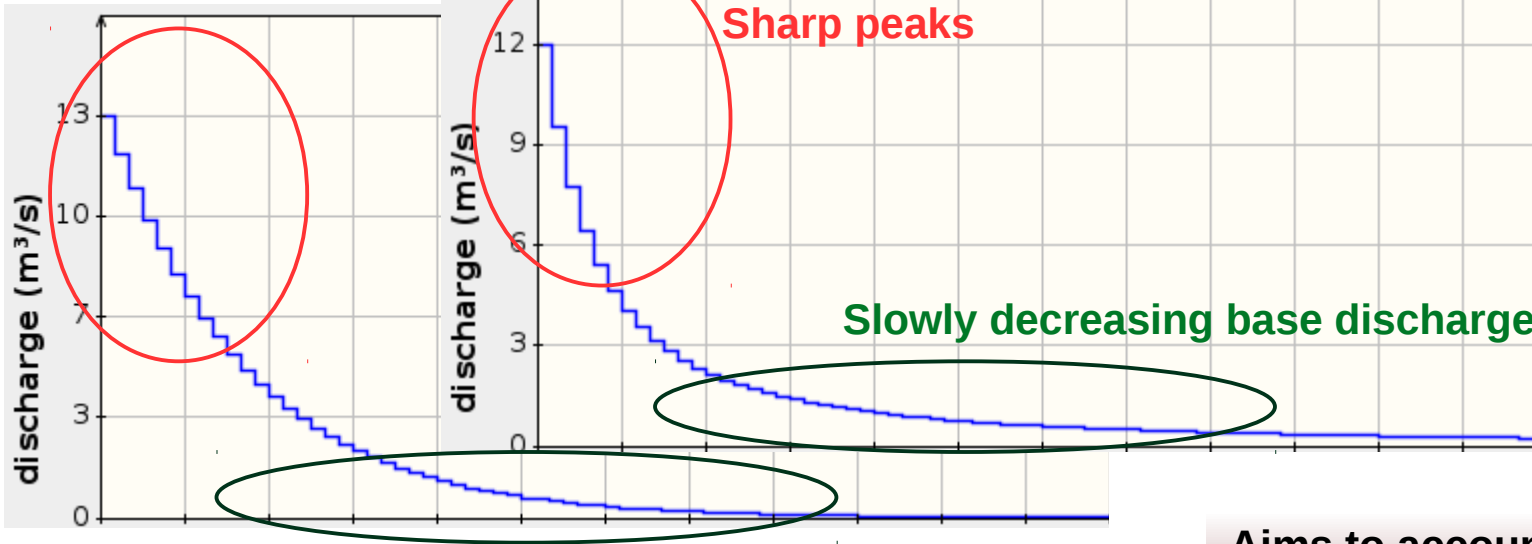
► Unit response

$$\omega(t) = \frac{\alpha \tau_0^\alpha}{(\tau_0 + t)^{1+\alpha}} \quad 0 < \alpha < 1$$



Tcinf decay

Exponential decay



Aims to account for multiple transfer time scales in hydrosystems
→ Dual flow behaviour

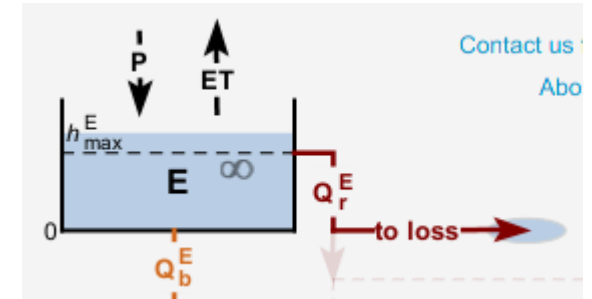
Step by Step example : transfer laws

Infinite characteristic time configuration

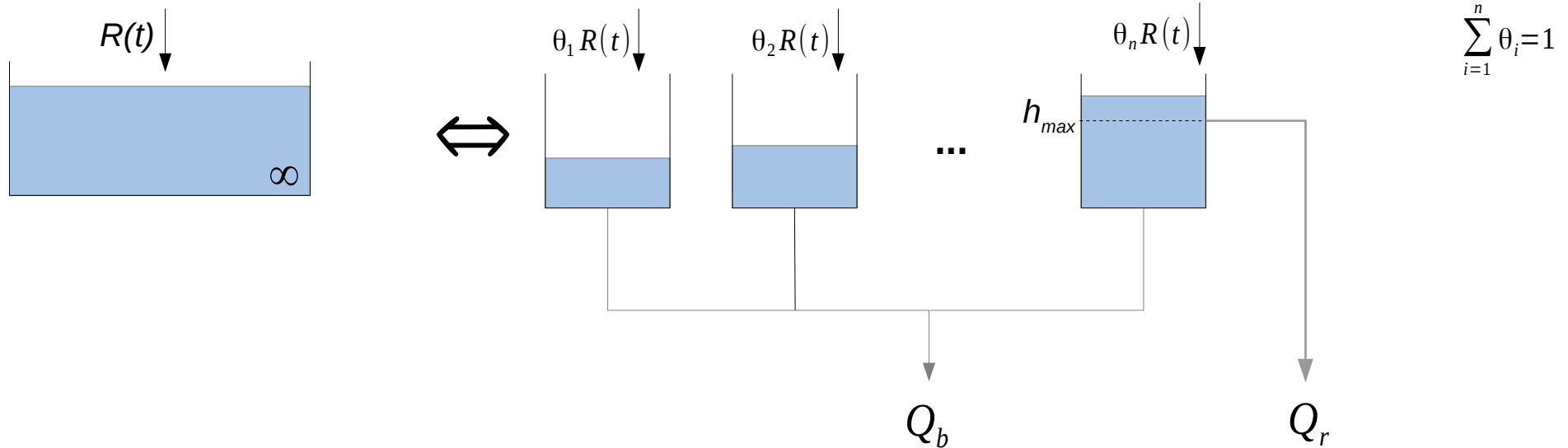
► Unit response

$$\omega(t) = \frac{\alpha \tau_0^\alpha}{(\tau_0 + t)^{1+\alpha}} \quad 0 < \alpha < 1$$

$$Q_b = R \otimes \omega(t)$$



► Volume higher than threshold h_{max} triggers direct overflow Q_r



Amounts to partitioning reservoir C into sub-reservoirs with linear discharge law, running in parallel.

Step by Step example : objective function

Performance measure

Volume Error (VE)
Nash-Stucliffe efficiency (NSE)
Kling-Gupta efficiency (KGE)

Balance error

Use 1 or a combination of 2
objective functions

Dataset

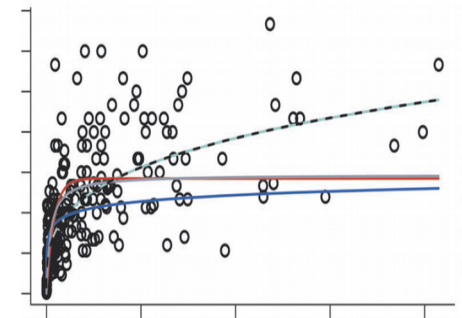
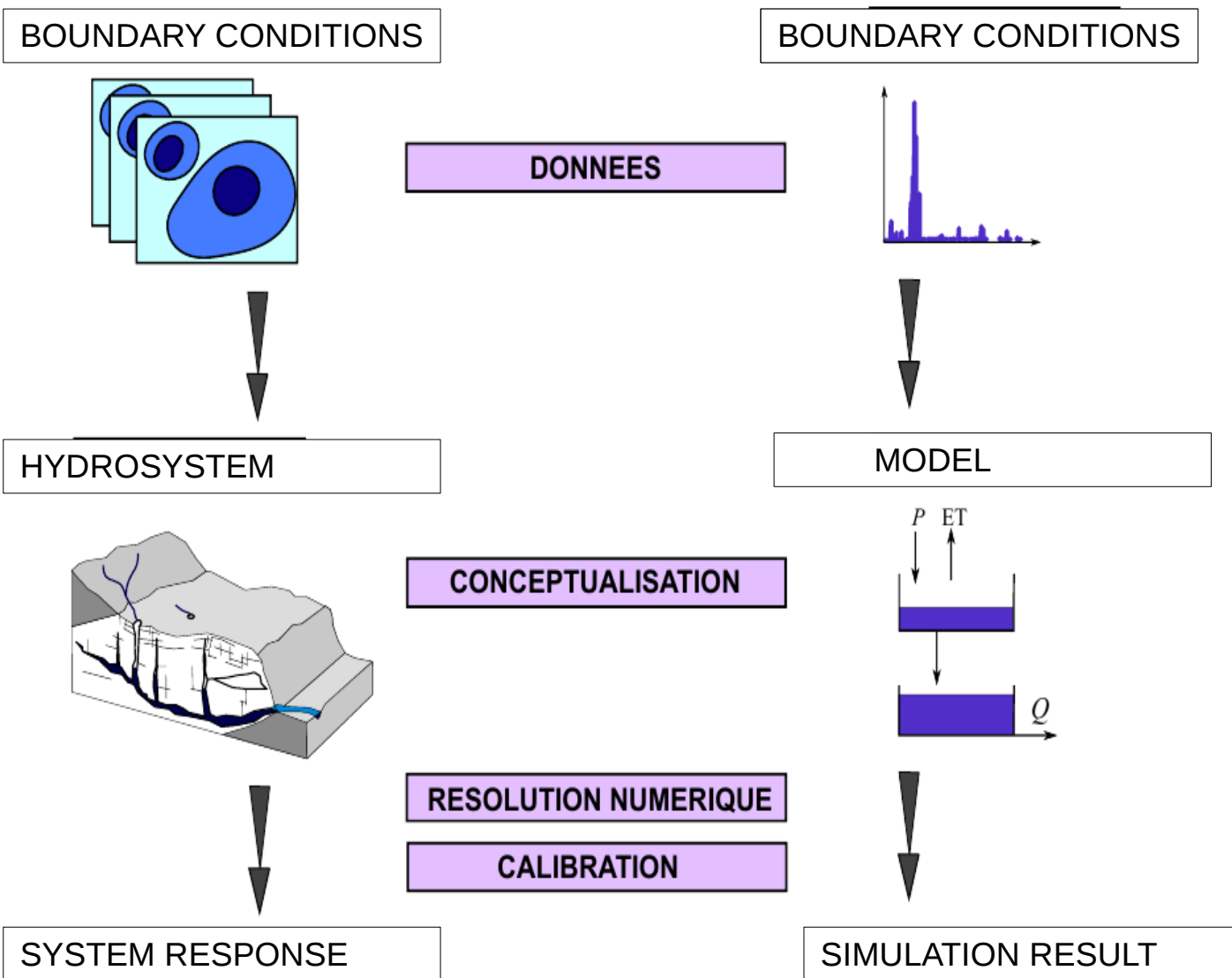
- ✓ Entire dataset $Q(t)$
- ✓ Peak flow $Q(t) > Q_{min}$
- ✓ Base discharge $Q(t) < Q_{max}$

Variable

- ✓ Discharge or equivalent water level
- ✓ $\sqrt{\cdot}$, $\log(\cdot)$

Performance measures drive the calibration process
Which characteristics of the measured signal do you
want to reproduce ?

Step by Step example : your model can't perfectly fit the data



**Errors occur at all stages
of the modelling
process**

**There's no unique
solution to the
modelling problem
=
EQUIFINALITY**

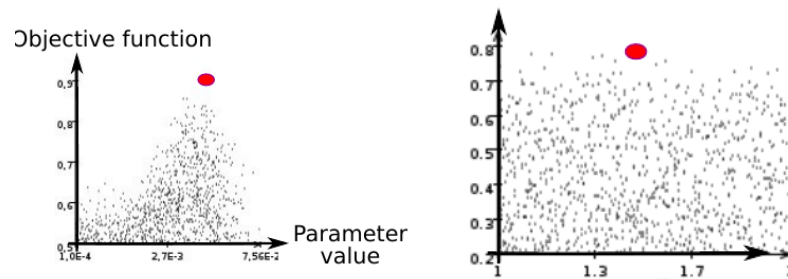
**Non-optimal parameters
set may still provide
some interesting
information**

Step by Step example : relevant realizations approach

→ In KarstMod, all simulations that comply $WOBJ > WOBJ_{\min}$ are retained for analysis

1/ At first, set a low minimal performance measure $WOBJ_{\min}$

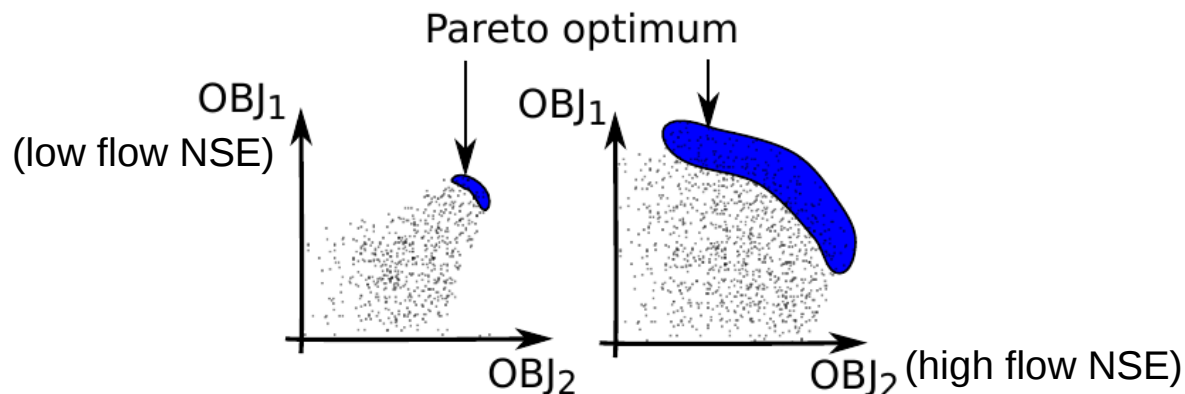
→ check parameter bounds & optimum



→ check key parameters
(sensitivity indexes)

→ ...

→ check possible conflicts between signal characteristics



Final choice of wobj

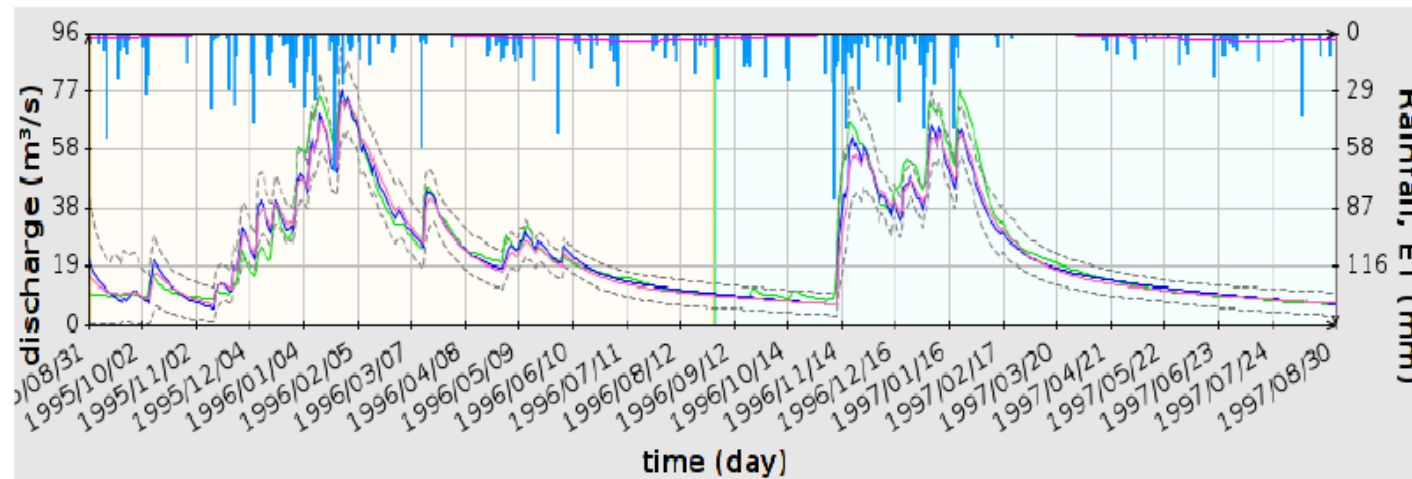
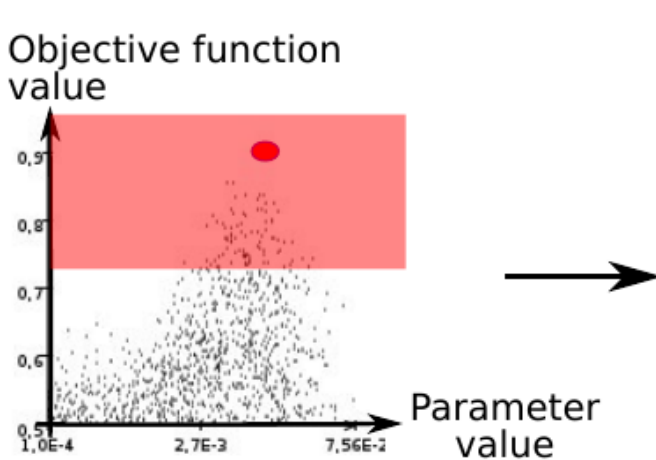
Set model structure &
transfer laws

Step by Step example : relevant realizations approach

→ In KarstMod, all simulations that comply $WOBJ > WOBJ_{\min}$ are retained for analysis

1/ At first, set a low minimal performance measure $WOBJ_{\min}$

2/ When model structure is deemed adequate, use higher $WOBJ_{\min}$



- simulation resulting from optimal parameter set (best wobj)
- min & max Q values from set of acceptable simulations
- most likely Q value based on set of acceptable simulations
- 95 % confidence bounds based on acceptable simulations

GLUE methodology : Beven 1992

APPENDIX

PERFORMANCE MEASUREMENTS

Nash-Sutcliffe efficiency

$$NSE = 1 - \frac{\sum (Q_{OBS} - Q_i)^2}{\sum (Q_{OBS} - \overline{Q_{OBS}})^2}$$

- $\in]-\infty, 1]$
- $Q_{obs} = Q_{obs} \Rightarrow NSE = 0$

NSE provide a relative quantification of model performance

more pertinent reference simulations can be used

NSE = 0.8

$\Leftrightarrow$

erreur quadratique moyenne $\div$ 5
As compared to reference simulation

NSE may be low even though the general shape of $Q(t)$ is ok

NSE will be higher if the reference model is bad (high variability of $Q(t)$)

